

Technical Memorandum: Delta Risk Management Strategy (DRMS) Phase 1

Topical Area:

Emergency Response and Repair Final

Prepared by: URS Corporation/Jack R. Benjamin & Associates, Inc.

Prepared for:
California Department of Water Resources (DWR)

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Subject: Delta Risk Management Strategy

Final Phase 1 Technical Memorandum – Emergency Response and

Repair

Dear Mr. Bagheban:

We are providing the final Emergency Response and Repair Technical Memorandum (TM) (dated May 30, 2008) for Phase 1 of the Delta Risk Management Strategy (DRMS) project. Members of the Steering Committee's Technical Advisory Committee and agency staff reviewed the second draft TM, and their comments were incorporated before the CALFED Independent Review Panel (IRP) review of the June 26, 2007, draft of the Risk Analysis Report. This final version of this TM addresses the IRP comments provided on the emergency response and repair sections of the Risk Analysis Report.

This TM was prepared by Rick Rhoads, Ingrid Maloney, H. Frank Du, and Curtis Loeb (Moffat & Nichol). This technical memorandum was reviewed by Drs. Said Salah-Mars (URS) and Marty McCann (JBA). Internal peer review was provided in accordance with URS' quality assurance program, as outlined in the DRMS project management plan.

Sincerely,

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Preamble

In response to Assembly Bill (AB) 1200 (Laird, chaptered, September 2005), the California Department of Water Resources (DWR) authorized the Delta Risk Management Strategy (DRMS) project to perform a Risk Analysis of the Sacramento–San Joaquin Delta (Delta) and Suisun Marsh (Phase 1) and to develop a set of improvement strategies to manage those risks (Phase 2).

AB 1200 amends Section 139.2 of the Water Code to read: "The department shall evaluate the potential impacts on water supplies derived from the Sacramento–San Joaquin Delta based on 50-, 100-, and 200-year projections for each of the following possible impacts on the Delta:

- 1. Subsidence
- 2. Earthquakes
- 3. Floods
- 4. Changes in precipitation, temperature, and ocean levels
- 5. A combination of the impacts specified in paragraphs (1) to (4) inclusive."

AB 1200 also amended Section 139.4 to read: "(a) The Department and the Department of Fish and Game shall determine the principal options for the Delta. (b) The Department shall evaluate and comparatively rate each option determined in subdivision (a) for its ability to do the following:

- 1. Prevent the disruption of water supplies derived from the Sacramento–San Joaquin Delta.
- 2. Improve the quality of drinking water supplies derived from the Delta.
- 3. Reduce the amount of salts contained in Delta water and delivered to, and often retained in, our agricultural areas.
- 4. Maintain Delta water quality for Delta users.
- 5. Assist in preserving Delta lands.
- 6. Protect water rights of the "area of origin" and protect the environments of the Sacramento–San Joaquin river systems.
- 7. Protect highways, utility facilities, and other infrastructure located within the Delta.
- 8. Preserve, protect, and improve Delta levees...."

To meet the requirements of AB 1200, the DRMS project has been divided into two parts. Phase 1 involves the development and implementation of a Risk Analysis to evaluate the impacts of various stressing events on the Delta. Phase 2 evaluates the risk reduction potential of alternative options and develops risk management strategies for the long-term management of the Delta.

As part of the Phase 1 work, 12 technical memoranda (TMs), which address individual topical areas, and one risk report have been prepared. This TM addresses the emergency response and repair issues that are considered in Phase 1. The TMs and the topical areas covered in the Phase 1 Risk Analysis are as follows:



- 1. Geomorphology of the Delta and Suisun Marsh
- 2. Subsidence of the Delta and Suisun Marsh
- 3. Seismology of the Delta and Suisun Marsh
- 4. Climate Change in the Delta and Suisun Marsh
- 5. Flood Hazard of the Delta and Suisun Marsh
- 6. Wind-Wave Hazard of the Delta and Suisun Marsh
- 7. Levee Vulnerability of the Delta and Suisun Marsh
- 8. Emergency Response and Repair of the Delta and Suisun Marsh Levees
- 9. Hydrodynamics, Water Quality, and Management and Operation of the Delta and Suisun Marsh (Water Analysis Module)*
- 10. Ecosystem Impacts to the Delta and Suisun Marsh
- 11. Impact to Infrastructure of the Delta and Suisun Marsh
- 12. Economic Consequences to the Delta and Suisun Marsh

The work products described in all of the TMs are integrated in the DRMS Risk Analysis. The results of the Risk Analysis are presented in a technical report referred to as:

13. Risk Analysis Report

Taken together, the Phase 1 TMs and the Risk Analysis Report constitute the full documentation of the DRMS Risk Analysis.

The Business-as-Usual Delta and Suisun Marsh: Assumptions and Definitions

To carry out the DRMS Phase 1 analysis, it was important to establish some assumptions about the future "look" of the Delta. To address the challenge of predicting the impacts of stressing events on the Delta and Suisun Marsh under changing future conditions, DRMS adopted the approach of evaluating impacts absent major future changes in the Delta as a baseline. Thus, the Phase 1 work did not incorporate or examine proposals for Delta improvements. Rather, Phase 1 identified the characteristics and problems of the current Delta (as of 2005), with its practices and uses. This approach, which allows for consideration of pre-existing agreements, policies, funded projects, and practices, is referred to as the "business-as-usual" (BAU) scenario. Defining a BAU Delta is necessary because one of the objectives of this project is to estimate whether the current practices of managing the Delta (i.e., BAU) are sustainable for the foreseeable future. The results of the Phase 1 Risk Analysis based on the BAU assumption not only maintained continuity with the existing Delta, but also served as the baseline for evaluating the risk reduction measures considered in Phase 2.

The existing procedures and policies developed to address "standard" emergencies in the Delta, as covered in the BAU scenario, do not cover some of the major (unprecedented) events in the Delta that are evaluated in the Risk Analysis. In these instances, prioritization of actions is based on (1) existing and expected future response resources and (2) the highest value of recovery/restoration given available resources.

^{*}Two separate topical areas—the Hydrodynamics topical area and the Water Management topical area—were combined into one TM because of the strong interaction between them. The resulting TM is referred to as the Water Analysis Module (WAM).

This study relied solely on available data. In other words, the effects of stressing events (changing future earthquake frequencies, future rates of subsidence given continued farming practices, the change in the magnitude and frequency of storm events, and the potential effects of global warming) on the Delta and Suisun Marsh levees were estimated using readily available engineering and scientific tools or based on a broad and current consensus among practitioners. Using the current state of knowledge, the DRMS project team made estimates of the future magnitude and frequency of occurrence of the stressing events 50, 100, and 200 years from now to evaluate the change in Delta risks into the future.

Because of the limited time available to complete this work, no investigation or research was conducted to supplement the current state of knowledge.

Perspective

The analysis results presented in this TM do not represent the full estimate of risk for the Delta and Suisun Marsh. The full estimate of risk is the probable outcome of the hazards (earthquake, floods, climate change, subsidence, wind waves, and sunny day failures) combined with the conditional probability of the subject outcome (levee failures, emergency response, water management, hydrodynamic response of the Delta and Suisun Marsh, ecosystem response, and economic consequences) given the stressing events. A full characterization of risk is presented in the Risk Analysis Report. In that report, the integration of the initiating (stressing) events, the conditional probable response of the Delta levee system, and the expected probable consequences are integrated to develop a complete assessment of risk to the Delta and Suisun Marsh. In this context, the subject of this TM is one element of the Risk Analysis.



Table of Contents

1.	Introduction					
2.	Objective	1				
3.	Assumptions and Limitations	1				
3.1	Business as Usual	. 1				
3.2	Material Source	. 1				
3.3	Applicability to Years 2050, 2100, and 2200	. 2				
3.4	Emergency Preparedness	. 2				
3.5	Operability after a Seismic Event	. 2				
3.6	Other Assumptions	. 2				
4.	Emergency Response and Repair Model	3				
4.1	General	. 3				
4.2	Simulation Tool	. 4				
4.3	Model Database	. 4				
4.4	Repair Types					
4.5	Island and Work Type Prioritization (Work Order)					
4.6	Sequence Definition / User Input	. 8				
4.7	Secondary Breaches on Non-Flooded Islands	11				
4.8	Continuing Damage on Flooded Islands	11				
4.9	Repair Rates	12				
4.10	Ongoing Flood-Fighting Activities	14				
4.11	Dewatering	15				
4.12	Cost	15				
5.	Sample Input and Output	15				
5.1	Sequence 1	15				
5.2	Sequence 2	19				
5.3	Sequential Output in Text File Format					

Tables	
4-1	Island Sectors
4-2	Sequence Description (Initial Breaches and Damages)
4-3	Assignment of Islands to Island Priority Groups
4-4	Priorities for Repair of Initial Breaches and Damages
4-5	Internal Ordering of Input Data
4-6	Production Rates by Time (SRRQ and Others, Marine-Based)
4-7	Production Rates by Time (Local Quarries, Land-Based)
4-8	Production Rates by Activity (Placing Rates)
5-1	Sequence 1 Damage Input
5-2	Sequence 1 Island Priority Group Input
5-3	Sequence 1 Repair Order Prioritization Input
5-4	Damage Summary (Internal Array) for Sequence 1
5-5	Sequence 1 Output
5-6	Output to Water Quality Model for Sequence 1
5-7	Sequence 2 Damage Input
5-8	Sequence 2 Island Priority Group Input
5-9	Sequence 2 Repair Order Prioritization Input
5-10	Damage Summary (Internal Array) for Sequence 2
5-11	Sequence 2 Output
5-12	Output to Water Quality Model for Sequence 2
A-1	Soil Erodibility Parameter Ranges
Figures	
4-1	Division of Each Island into Eight Sectors
5-1	Appearance of Sequential Outputs (for 2 Sequences)
5-2	Appearance of Sequential Outputs to Water Quality Module (for 2 Sequences)
A-1	Erosion Rate Envelope
_	.

Appendices

A Development of Wind-Wave Erosion Parametric Equations

List of Acronyms and Abbreviations

CEQA California Environmental Quality Act

cfs cubic feet per second

DRMS Delta Risk Management Strategy
DWR Department of Water Resources

ER&R Emergency Response and Repair

Lb breach length

MHHW mean high higher water

MLLW mean low lower water

NEPA National Environmental Policy Act

RT repair type

SRRQ San Rafael Rock Quarry

tpd tons per day

1. Introduction

The Emergency Response and Repair (ER&R) model has been developed as part of the Delta Risk Management Strategy (DRMS) project. This technical memorandum describes the model, its objectives, assumptions and limitations, its required inputs, and the outputs that will be generated by the module.

2. Objective

The ER&R model objective is to estimate the time and material required, and the associated costs, to stabilize damaged levee sections, prevent further damage, close breaches and dewater flooded islands following an event. An event (or sequence) is defined as a flood, seismic, or other event that results in any number of levee breaches and/or damaged levee sections. The event's consequences in terms of levee damage and failures are evaluated as part of the DRMS risk analysis and are passed on to the ER&R module. The ER&R model must be applicable for the range of events/sequences that will be modeled in the DRMS study, while also considering the effect on emergency response capability resulting from flood-fighting activities during the winter months.

Following an event, depending on the repair prioritization scheme, breaches may be capped and/or filled, while damaged levee sections require remediation to prevent further breaches. In the case of flooded islands, where levees have been breached, the interior slope of damaged or intact levee sections may be protected against erosion resulting from exposure to wind-driven wave action. Flooded islands may be dewatered after breach closure.

The ER&R model focuses on post-event actions only. Seasonal flood-fighting activities are not explicitly modeled, though the model allows for a reduction in emergency response capacity during the time of the year when one would expect non-event-related flood-fighting actions on non-flooded islands to be ongoing. As such, these activities would divert resources from the emergency operations.

3. Assumptions and Limitations

3.1 Business as Usual

It is assumed that rock placement will be the exclusive means of stabilizing damaged levees and breaches. It is also assumed that the normative approach used in the past will be followed: capping of breach ends to stabilize the breach before attempts are made to close it and placement of erosion protection on the interior levee slopes of flooded islands. Deviation from the normative approach is possible and, depending on the repair prioritization scheme, not all or any of these measures may be carried out on a particular island.

3.2 Material Source

It is assumed that the San Rafael Rock Quarry (SRRQ) is the primary source of material and the only source of material for marine-based activities. Currently, the SRRQ, located in San Rafael, California, and owned by The Dutra Group, is the primary supplier of quarry products for the Delta. The SRRQ is the only quarry located in northern California

with direct loading access to barges. Consequently, the quarry possesses a significant advantage over competing quarries in its ability to directly load barges with product for delivery to the Delta, and the economy of scale this advantage offers. Placement of erosion protection and repair of erosion damage can be carried out from land, if access permits. In this case, material will be sourced from local quarries.

3.3 Applicability to Years 2050, 2100, and 2200

It is assumed that the SRRQ will be in operation for the next 200 years, even though the quarry's rock supply is more consistent with about 52 years of continued operation.

3.4 Emergency Preparedness

The State has improved its pre-event emergency preparedness, and will likely continue such improvements as a result of lessons learned from the recent Jones Tract levee breach, as well as the DRMS findings. However, it is believed such measures will have a limited effect on overall emergency response and repair durations calculated by this model, since this model already presumes an effective emergency preparedness status is in place. Furthermore, as the magnitude of sequence damage increases, it is believed the effect of emergency preparedness on overall repair durations diminishes. Therefore, the model does not quantitatively account for such emergency preparedness preparations beyond the assumption that such preparations enable the model to meet the emergency response and repair production rates presumed within.

3.5 Operability after a Seismic Event

The SRRQ, as well as all other infrastructure, will remain operational after a seismic event. For instance, after a seismic event in the Bay Area, there may be access constraints for the barges if bridges have collapsed, but it has been assumed that there will be no access constraints.

3.6 Other Assumptions

- Within days of a sequence of levee breaches, local regulations will be eased or set aside to allow the SRRQ to operate on a 24-hour basis.
- Sufficient transportation equipment (i.e., deck barges, scows, and tugs) can be made available immediately, so that material supply capacity remains the constraint.
- Resources (i.e., materials and equipment) are assumed to be available and will not be compromised by demands outside the Delta that occur as a result of the same seismic event. Damage that occurs to assets other than levees will not put a demand on resources required to support levee breach repairs.
- Additional damage resulting from earthquake aftershocks is not considered.
- There are no constraints on dewatering resources.

The following factors are not explicitly accounted for in the emergency response and repair model, yet they may impact the analysis results:

• The time required to put contracts into place may be significant and will vary from event to event.

- It may not be possible for The Dutra Group to obtain permits to build a second loading facility in within 90 days. State/federal officials may need to step in and waive the typical permitting process (California Environmental Quality Act [CEQA]/National Environmental Policy Act [NEPA]). Additionally, SRRQ neighbors may hold up the process if they do not see events in the Delta as an impact on them.
- It may take longer than 180 days to bring other sources of material on line. The State will have to make the decision when to call in help from non-local sources, such as Catalina Island, Canada, or Mexico.
- After a seismic event, there may be numerous projects competing for the same resources. The State will have to prioritize all competing projects.

4. Emergency Response and Repair Model

This section summarizes the model for the emergency response and repair for the Delta Risk Management Strategy.

4.1 General

4.1.1 Event-Related Response and Repair

As part of the DRMS study, a risk model is being developed, modeling the potential occurrence of events (floods, earthquakes, etc.) that may lead to levee failures and/or damaged levee segments. The risk model will consider the complete set of levee damage and/or failure sequences that could occur and their likelihood of occurrence.

Following an event, there may be a number of islands flooded as a result of one or more levee breaches on that island. In addition to levee breaches, there may be levee sections that have been damaged, but which have not been breached. A non-flooded island is one that does not experience a levee breach following an event. However, non-flooded islands may have damaged levee sections that require remediation to avoid a breach at a later time. Furthermore, each flooded island flooded is susceptible to interior levee slope erosion resulting from exposure to wind-driven wave action. Such erosion may occur on both damaged and non-damaged levee sections. Erosion rates depend on the wind vulnerability of a particular section ("segment") of levee, which varies based on the fetch and exposure of that section to the predominant wind direction.

Given a sequence that identifies a set of levee breaches and/or damage throughout the Delta, the ER&R model makes an assessment of the ability to respond. The assessment will address the following factors key to estimating the amount of time required for achieving a return to normal operations (i.e., normal water export):

- Prevention of continuing damage (remediation of damaged sections of levee, capping of breached levee ends, and interior levee protection)
- Breach closure
- Dewatering of flooded islands

The analysis considers gross quantities of material required for repairing damage and closing breaches but does not differentiate among material types.

4.1.2 Non-Event-Related Response and Repair

Depending on an event's time of year, there may be other flood-fighting activities taking place in the Delta that are not related to an event. These activities may divert resources from the event-related response activities.

4.2 Simulation Tool

The emergency response and repair module was developed as a simulation model, using the simulation software package Extend, which is an industry-standard, general-purpose simulation tool that can be used to model a large variety of processes. Extend is a powerful object-oriented simulation tool that uses the MOD-L programming language, and has been employed on many projects that required probabilistic assessment to determine various outcomes' risk/probability.

The model employs Extend's capability of combining discrete event simulation with continuous simulation flow architecture. In the discrete event simulation items are generated, each item representing a specific repair that must be carried out for the particular sequence being analyzed. The number of items required for a particular sequence depends on the number of individual breaches and damaged sections on the affected islands, plus all eight levee segments on flooded islands (see Section 4.3, Table 4.1 and Figure 4.1) that are susceptible to interior slope erosion, and the repair work order that has been specified for that sequence. Extend flow architecture is used to model the production rates, which represent the combination of production capacity of the quarries and transportation capability.

The emergency response and repair simulation model consists of a number of blocks, as follows:

- Model Database
- Read and Organize Input Data
- Set up Simulation Items to Track Each Type of Repair Item
- Continuing Damage
- SRRQ Rock Supply
- Delta Quarries Rock Supply
- Ongoing Flood-Fighting Activities
- Repairs
- Dewatering
- Cost
- Output to Water Quality Model

4.3 Model Database

The model database consists of the Main Database and the Damage and Repair Progression Database.

The Main Database includes the main parameters associated with each island in the legal Delta and Suisun Marsh. The islands and their IDs match those from the URS GIS Database. Each island is divided into eight sectors that correspond to the eight compass directions (N, NE, E, SE, S, SW, W, and NW), as shown on Figure 4-1 and summarized in Table 4-1. The database includes levee cross sectional parameters, perimeter length, and fetch associated with each of the eight island segments.

Table 4-1 Island Sectors

N	0	$337.5 < \theta \le 360, 0 < \theta \le 22.5$
NE	45	22.5< θ <= 67.5
Е	90	67.5< θ <= 112.5
SE	135	112.5< θ <= 157.5
S	180	$157.5 < \theta \le 202.5$
SW	225	$202.5 < \theta \le 247.5$
W	270	$247.5 < \theta \le 292.5$
NW	315	$292.5 < \theta <= 337.5$

User-selected sequence input is processed and summarized in the Continuing Damage and Repair Progression Database, which stores all damage information related to the sequence. The database is updated to record changes to damaged volume, breach length, and damage status as time progresses, to reflect continuing damage and ongoing repair activities. Damage continues on each breach in accordance with the input breach growth rate, and on each damaged or intact levee located on a flooded island in accordance with erosion rates, as long as repair works have not been initiated on that particular levee section. As soon as breach-end capping commences, the breach growth rate is set to zero; as soon as repair starts on a damaged levee segment on a flooded island, the erosion rate is set to zero.

The database stores the priorities for each repair, the priorities are computed according to the preferences input by the user for that sequence. Repair start and end times are recorded as they occur, as are the quantity of rock placed, volume of water pumped, and associated cost. These parameters are recorded for each island segment and for the island as a whole.

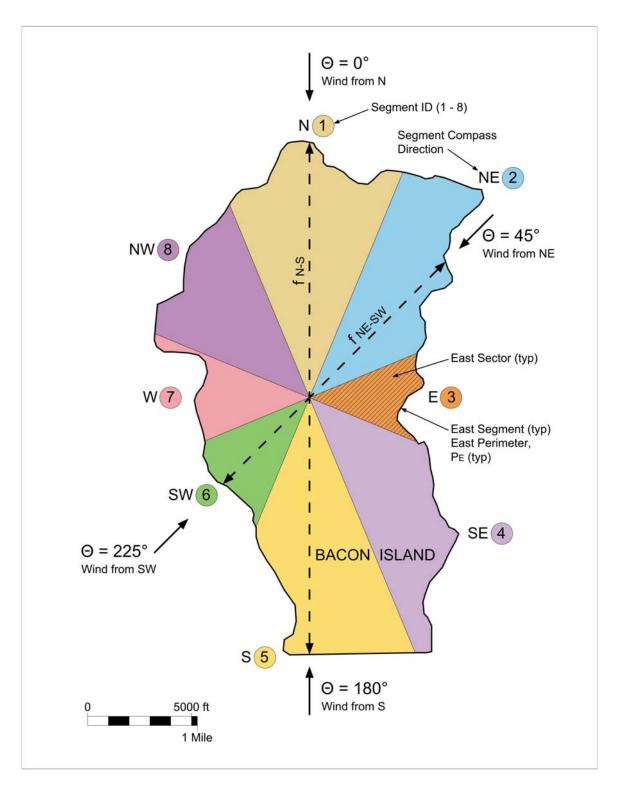


Figure 4-1 Division of Each Island into Eight Sectors

4.4 Repair Types

There are six repair types:

- RT1 repair post-event, non-breach damage on non-flooded island
- RT2 protect the levee interior slopes on a flooded island against wind-wave damage, or repair damage if it has already occurred
- RT3 repair post-event, non-breach damage on flooded island
- RT4 stabilize breached levees by capping the levee ends at the breach
- RT5 breach closure
- RT6 island dewatering

During the dry season, erosion protection and/or repair of damage resulting from erosion (repair type RT2) can be performed from land, using rock produced at local quarries transported and dumped onto the interior slope by truck. Dry-season RT2 is limited to those levees that have road access. Although the model differentiates between those islands that have land access and those that do not, it does not differentiate between roads that are in good condition and those that require strengthening to allow the land-based work to proceed. Resource and time requirements to strengthen or construct access roads to allow the truck transit associated with land-based repair are not included in the material, cost, and time estimates produced by the ER&R model. Furthermore, the model does not include any temporary or permanent raising the levee elevation in the case of erosion protection or repair.

As mentioned in Section 2, ER&R model response and repair actions represent postevent actions only. Seasonal flood-fighting activities are not modeled, though the model allows for a reduction in emergency response capacity during the time of the year when non-event-related flood-fighting actions on non-flooded islands might be ongoing.

4.5 Island and Work Type Prioritization (Work Order)

A significant level of flexibility is provided in the ER&R model in terms of developing the repair program (work order) for a given sequence. This level of flexibility allows for complete definition of a work order to the point where the order of completion of tasks is defined across islands and repair types. The module provides a level of flexibility that is consistent with the level of flexibility that can reasonably be defined and implemented in the field.

Islands identified in a sequence as having been breached and or damaged are sorted into priority groups. Islands within a priority group will have the same priority and the same repair work order. There can be as few as one group (all islands have equal priority and the same repair work order) or there can be as many groups as there are permutations of number of islands and repair work order. This scheme allows the user to completely define the work order, and to drop certain repair types, if desired.

4.6 Sequence Definition / User Input

The required user input is provided as three separate tables, similar to Tables 4-2, 4-3, and 4-4, which were generated for a randomly selected sequence.

4.6.1 Sequence Description

The first table defines a sequence by using the number and lengths of the breaches and damaged sections. Levee segments are defined with the goal of facilitating identification of levee damage and susceptibility to erosion. For each island, a geometrical center was determined and lines drawn from this center at equal angles to delineate eight sectors: N, NE, E, SE, S, SW, W, and NW (Figure 4-1). The eight levee segments are the perimeters of each sector.

The first row of Table 4-2 gives the sequence ID and the day of the year (1 through 365) on which the event occurs. Damage is defined in the successive rows of the table by providing the island ID, the segment number (1 through 8), and the damage state (1=damaged, 2=breached) for each sector of a levee that sustains damage in the event. The length of the damaged (or breached) section, and slump height (or breach growth rate), are also defined. The time at which the breach occurs is given, providing a means for entering the possibility of a secondary breach occurring on a damaged section of levee.

Table 4-2 Sequence Description (Initial Breaches and Damages)

Sequence Id Day Of Year

8110

Sequence 1u	Day Of Teal				
8110	0				
Island Id	Segment	Damage State (1)	Length (2)	Slump Height / Breach Growth Rate ⁽³⁾	Time (Days)
3	8	2	300	4	0
10	2	1	500	36	0
2	3	2	175	4	0
8	1	1	675	30	0
8	1	1	350	30	0
7	6	1	800	42	0
20	4	2	150	4	0
20	5	2	225	4	0
5	5	2	250	4	0
10	1	1	425	30	0
20	6	1	600	24	0
8	2	1	100	30	0
10	2	2	100	4	120

⁽¹⁾ damage state=1 means non-breach damage, damage state=2 means breach

Flooded islands are shown shaded (typical all tables). Island 10 is shown as a non-flooded island, as this is the initial condition. At 120 days, part of the damaged section on segment 2 breaches, flooding the island (provided the damage has not been fixed by that time).

The data in Table 4-2 can be listed in any order (i.e., the order does not need to be consecutive island order). An island may be listed multiple times in the case of multiple



⁽²⁾ length = damage length or breach length (ft) depending on damage state

⁽³⁾ slump height (in) or breach growth rate (in/day) depending on damage state

breaches and/or damaged levee sections along one or more of the levee's eight segments. The multiple occurrences of an island do not have to be listed in consecutive order.

4.6.2 Island Prioritization

Island priority groups are defined in order, to allow for variations in work order prioritization among all the affected islands, while also allowing assignment of identical work order prioritization for similar islands. The island prioritization is defined for each sequence, although it may be likely that it will be identical for many, if not all, sequences.

Sequence Id	
8110 Island Id	Island Priority Group
3	1
2	3
5	2
7	2
8	1
10	1
20	2

Table 4-3 Assignment of Islands to Island Priority Groups

In this example there are three priority groups. Priority group 1 (highest priority) includes non-flooded and flooded islands. So does priority group 2 (medium priority). Priority group 3 (lowest priority) includes only one flooded island. The islands can be listed in any order in Table 4-3, but they may be listed only once and *only those islands that are affected in the current sequence should be listed in Table 4-3*

There is no significance to the order in which islands are listed in Tables 4-2 and 4-3. Because this sequence is the current test case for the model, a completely random listing was chosen to demonstrate the model's generality.

4.6.3 Repair Work Order / Prioritization

The prescribed order of carrying out the repair types RT1 through RT6 is defined for each island priority group via the input format of Table 4-4.

Sequence Id 8110						
Island Priority Group	RT1	RT2	RT3	RT4	RT5	RT6
1	1	2	2	2	3	1
2	1	0 (1)	4	0	5	2
3	1	0	7	6	6	0

Table 4-4 Priorities for Repair of Initial Breaches and Damages

⁽¹⁾ Opt not to protect interior slopes or to cap breaches on islands in Group 2 and opt not to protect interior slopes on islands in Group 3.

Priorities in Table 4-4 are user-defined across island priority groups and across repair types. This allows for any work order within an island priority group or across all damaged islands.

In this example, RT1 is to be completed on all damaged, non-flooded islands (starting with the islands in the highest priority group) before completing any other repairs. Repetition of a priority number implies that the repair type with the identical priority number should be completed on each island before moving on to the next island within the island's priority group. In the example, the second priority is to complete RT2-RT3-RT4 on island 3, then to do the same on island 8 and then on island 10 (it happens that both islands 8 and 10 are non-flooded and that they do not require repair types RT2, RT3 or RT4). Then, RT5 is to be completed on island 3, followed by islands 8 and 10 (which do not require RT5, but if they did, would be completed next).

Repair type RT6 (dewater island) is not part of the overall work order scheme as described above, but the entries in the column associated with RT6 allow the user to make the following decision for each island priority group:

- 0 =Island not to be dewatered (even when breaches have been fixed).
- 1 = Island to be dewatered as soon as all breaches have been fixed on the island, with the possibility that other, specified repairs may not have been completed.
- 2 = Island to be dewatered only after all specified repairs have been completed on the island.

4.6.4 Internal Ordering of Repair Types

Internally, the three sets of input presented in Tables 4-2 through 4-4 are converted into a matrix as shown in Table 4-5. The accumulated length of damages and breaches on each island is computed and listed as it plays a factor in the prioritization. This is because the grouping of islands into priority groups does not provide any detail on the order in which islands are to be completed within a group. Within a priority group, islands are selected based on amount (lineal feet) of damage, with the least damaged island being repaired first.

If resources allow, repair types RT2, RT3 and RT4 can be implemented simultaneously on a given island. Repair type RT5 can only commence once RT4 is completed. Selected repair types can be deleted from the work order for one, several, or all island priority groups.

Island	Priority Group	Row # In Damage Array	Cumulative Damaged Length (feet)	RT1	RT2	RT3	RT4	RT5
3	1	1	300	0	2001012	0	2001014	3001015
2	3	10	175	0	0	0	6003074	6003075
5	2	19	250	0	0	0	0	5002045
7	2	28	800	1002051	0	0	0	0
8	1	37	1,125	1001031	0	0	0	0
10	1	46	1,025	1001021	2001022	2001023	2001024	3001025
20	2	55	975	0	0	4002063	0	5002065

Table 4-5 Internal Ordering of Input Data

4.7 Secondary Breaches on Non-Flooded Islands

Non-flooded islands may have (1) intact levee sections and/or (2) damaged (slumped) levee sections. Intact levee sections are assumed to remain intact throughout the repair period that is simulated in the ER&R module. However, damaged sections can breach as a result of a storm event that causes overtopping and subsequent breach.

The levee fragility model estimates the fragility of damaged levee exteriors to wind waves or high flow rates. The occurrence of a secondary breach will be input to the ER&R model as part of the sequence definition (Table 4-2). The secondary breach must be defined by the same parameters that are required for initial breaches, including breach length (Lb) and breach growth rate. The time at which the secondary breach occurs must also be defined; thus, secondary breaches are identified by the last column in Table 4-2, where T>0 days. The breach will only actually occur if the damaged levee segment has not been repaired at that point in time.

4.8 Continuing Damage on Flooded Islands

Flooded islands have either (1) intact levee sections, (2) damaged (slumped) levee sections, or (3) breached sections, as well as exposed levee interiors of intact or damaged sections.

4.8.1 Exterior Damage

In the case of slumped levee sections on a flooded island, overtopping from the exterior (from an episodic storm) will not result in further breaches, since there are equal heights of water on both sides of the levee. However, exterior damage could occur as a result of waves breaking on the levee crest instead of on the riprap, as a result of an exterior episodic event. This would be an eroding type of damage (similar to interior slope erosion) over a short period of time, since it is episodic. Thus, it is likely to not be an important factor (it adds a little more to the material requirement of the already damaged levee section). This type of damage could be added during a second phase of the project.

4.8.2 Breach Growth

Breached sections will grow in length over time. The user inputs (via Table 4-2) the mean growth rate to the model. Breach growth that occurs after the island has flooded/equalized will be modeled as random, lognormally distributed with a mean and standard deviation equal to 10% of the mean value.

4.8.3 Wind-Wave Erosion

Wind-wave erosion on the levee's interior slopes will act upon both intact and damaged levee sections throughout the repair period that is simulated in the ER&R module. This erosion manifests itself as additional (continuing) damage on initially intact and damaged levee sections of flooded islands, resulting in larger quantities of rock being required when the repair of that section proceeds.

Levee interior slope erosion is modeled as follows:

- Sets of erosion curves, or parametric equations, (time vs. erosion) are defined within the ER&R module for each island sector. Development of the wind-wave erosion curves is presented in Appendix A.
- With each day that passes following flooding of the island, erosion damage is accumulated on the intact and damaged levee sections of each island sector.
- Erosion occurs at an equal rate along the entire levee perimeter of each island sector.
- The additional erosion acts on the levee width at mean higher high water (MHHW) (which is different for intact vs. damaged/slumped levee sections). When the levee's width has been eroded down to a threshold level of 6 feet (to be confirmed), it is assumed that the remaining portion of the levee fails, and the entire levee cross section above mean lower low water (MLLW) collapses and must be replaced for that specific levee segment.
- Accumulation of erosion damage stops when failure as defined above occurs or when laying of rock for protection of the levee interior commences. The amount of rock laid will be based on the amount required for the layer of protection plus the amount required to replace the eroded section.

4.9 Repair Rates

Since the rate of material supply is anticipated to be the governing constraint, the production rates (i.e., repair rates) are typically equal to the material loading rates.

Two potential sources of rock material are modeled. The SRRQ is assumed to be the primary material source for all marine-based repair activities, which includes all the repair types identified in Section 4.4. The second rock source comprises the numerous quarries in and near the Delta. The rock produced at these quarries is transported via truck; thus, use of local quarry rock is limited to the dry season and limited to those levees that have road access. Local quarry rock is used only for erosion protection and/or repair of damage resulting from erosion (repair type RT2).

It is assumed that one-half day will lapse before the contractor arrives at the initial levee failure and commences repair work. It is further assumed that another 2.5 days will lapse during which contracts for levee repair are put in place, although it is assumed that the contractor will start repair work during this period. Tables 4-6 and 4-7 summarize the assumed production rates by time at the SRRQ and at other quarries local to the Delta. Table 4-8 summarizes the production rates by activity for each phase of the repair and breach closure process. It is important to note that during a multi-damage and/or multi-breach sequence, the maximum production rates will be limited by the material supply rates stated in Tables 4-6 and 4-7 in combination with the possible placing rates stated in Table 4-8; however, the priority for repairing damage, protecting interior slopes versus capping levee ends and closing breaches must be specified in order to properly allocate the fixed resource of material supply.

For interior levee wind/wave protection efforts, depending on access to the flooded island, material may be sourced from quarries other than the SRRQ and delivered by truck. There are three significant constraints that might prohibit this:

- (1) If there is no vehicular bridge access to the island, trucking will not be possible.
- (2) During periods of elevated water levels in the Delta (December through May), the operation of trucks on levees is prohibited owing to concerns related to the potential for damage to the levees caused by heavy truck traffic.
- (3) When more than one section of levee is damaged or breached, truck access is assumed not possible.

Material supply varies over time as more equipment and infrastructure are added in response to the emergency. Tables 4-6 and 4-7 present the assumed increase in production rates over time for the SRRQ and local quarries, respectively.

The production rates quoted in Tables 4-6 and 4-7 beyond the first 10 days are based on presumed additional equipment and facility upgrades. These changes are assumed to be put into effect only if an order-of-magnitude estimate for the anticipated repair time exceeds certain values; i.e., only when the repair is of a magnitude that will make it worthwhile to increase capacity. Within each expansion phase, production capacity is expected to vary continuously. This variation is represented by a triangular distribution that has an expected, a low, and a high value, as shown in Tables 4-6 and 4-7.

Table 4-6 Production Rates by Time (SRRQ and Others, Marine-Based)

	Production Rate			
Days	Low	Expected	High	Remarks
0 to ½ day	0-tpd	0-tpd	0-tpd	Time required for contractor to
				commence work
½ to ~3 days	2,000-tpd	4,000-tpd	8,000-tpd	Time required to put repair
				contracts in place.
~3 to 10 days	4,000-tpd	10,000-tpd	12,000-tpd	Maximum SRRQ capacity with
				current equipment and
				configuration.
10 to 90 days	8,000-tpd	20,000-tpd	24,000-tpd	Addition of more mining
				equipment.
				Increase only if repairs are
				estimated to exceed 180 days
				duration.
90 to 180 days	20,000-tpd	40,000-tpd	48,000-tpd	Additional barge-loading facility.
				Increase only if repairs are
				estimated to exceed 360 days
				duration.
180+ days	30,000-tpd	50,000-tpd	58,000-tpd	SRRQ plus other marine sources.
				Increase only if repairs are
				estimated to exceed 720 days
				duration.

tpd = tons per day

 Table 4-7
 Production Rates by Time (Local Quarries, Land-Based)

		Production Rate		
Days	Low	Expected	High	Remarks
0 to ½ day	0-tpd	0-tpd	0-tpd	Time required for contractor to commence work
½ to ~3 days	1,300-tpd	1,800-tpd	6,200-tpd	Time required to put repair contracts in place.
~3 to 10 days	2,700-tpd	4,400-tpd	9,300-tpd	Maximum combined capacity (local quarries) with current equipment and configuration.
10 to 90 days	5,300-tpd	8,800-tpd	18,000-tpd	Additional mining equipment. Increase only if repairs are estimated to exceed 180 days duration.
90 to 180 days	13,000-tpd	18,000-tpd	37,000-tpd	Configuration modifications. Increase only if repairs are estimated to exceed 360 days duration.
180+ days	20,000-tpd	22,000-tpd	45,000-tpd	Further configuration modifications & additional mining equipment. Increase only if repairs are estimated to exceed 720 days duration.

tpd = tons per day

Table 4-8 Production Rates by Activity (Placing Rates)

Activity	Production Rate	Remarks
Levee Repair	3,200-tpd	Rate of 1 placing rig;
		max 1 placing rig per 2,000-ft
Interior Levee Protection		
Marine Access	3,200-tpd	Rate of 1 placing rig;
		max 1 placing rig per week's worth of
		activity
Land Access (trucking)	5,280-tpd	1 Truck (22-tons) every 5 minutes
_		(50- min-hr)
End Capping	1,600-tpd	Per breach
Levee Closure	4,800-tpd	Rate of 1 placing rig;
	_	max 1 placing rig per 300 ft

tpd = tons per day

4.10 Ongoing Flood-Fighting Activities

Seasonal flood-fighting activities on non-flooded islands are assumed to be ongoing during emergency operations, diverting resources and reducing response capacity during a limited time of the year.

The model allows for separate percent reductions in material supply, sourced from the SRRQ and the local quarries, that is available for the event-related emergency response.

The percent reduction can be set by the user and is based on the nominal daily production rate, which is 4,000 tons per day for the SRRQ and 1,800 tons per day for the local quarries. The default value is arbitrarily set to 25% for both SRRQ and local quarries. DWR input is required to finalize these values, such that realistic levels of resources are detracted to cover the flood-fighting activities. The model assumes that flood-fighting activities occur from December through March.

4.11 Dewatering

Dewatering operations will commence at the time of island closure or completion of all repairs on a flooded island (depending on the user input for the sequence—see Section 4.6). It is assumed that pump installation commences several days ahead of the anticipated closure of the island; thus, no lag time is assumed between island closure (or completion of repairs) and the start of pumping. Pumping rates are based on the assumption that only 42" pumps will be utilized and that these pumps operate at 80% efficiency, resulting in 107 cubic feet per second per pump. One pump will be allocated for every 20,000 acre-ft to be dewatered; therefore, the number of pumps is related to the volume of water to be pumped. The total pump rate is reduced by 50 cubic feet per second to account for seepage effects. These assumptions are based on a review of Jones Tract data.

4.12 Cost

Cost is computed based on \$55/ton of material placed and \$35/acre-ft of water pumped. The two unit rates given include the cost of labor, equipment, and materials.

5. Sample Input and Output

This section presents sample input and output for two sequences. The first sequence includes a number of breaches and damaged sections on seven islands. The second sequence includes a single breach on each of 10 islands, all islands having equal priority.

5.1 Sequence 1

The first sample sequence (sequence # 8001) involves seven impacted islands. A number of the islands have multiple breaches and/or damaged sections. The islands belong to three island priority groups. Island 10 is further expected to experience a secondary breach on its segment 2 on day 120, if the damaged section on that segment is not repaired by then. Tables 5-1 through 5-3 present the input (damage, assignment to island priority groups, and repair work order prioritization for each island priority group). Table 5-4 presents the internal Damage Summary array, which keeps track of the repairs and their priorities. The main output from the ER&R model is presented in Table 5-5—it gives summaries for the sequence and for each island (completion time for repairs and dewatering, quantity of rock placed, dewatering pump rate, number of pumps used simultaneously, and total cost). The output that is passed on to the Water Quality model is presented in Table 5-6—it presents a summary line for each flooded island as well as for each segment on that island (completion time for all repairs, for breach repairs only and for dewatering, and dewatering pump rate).

Table 5-1 Sequence 1 Damage Input

Sequence Id	Day Of Year				
8001	200				
				Slump Height /Breach	
		Damage	Length	Growth Rate	Time
Island Id	Segment	State	(Feet)	(Inches)	(Days)
3	8	2	300	4	1
10	2	1	500	36	1
2	3	2	175	4	1
8	1	1	675	30	1
8	1	1	350	30	1
7	6	1	800	42	1
20	4	2	150	4	1
20	5	2	225	4	1
5	5	2	250	4	1
10	1	1	425	30	1
20	6	1	600	24	1
8	2	1	100	30	1
10	2	2	100	4	120

 Table 5-2
 Sequence 1 Island Priority Group Input

Sequence Id	
8001	
	Island
	Priority
Island Id	Group
3	1
2	3
5	2
7	2
8	1
10	1
20	2

 Table 5-3
 Sequence 1 Repair Order Prioritization Input

Sequence						
Id						
8001						
Island Priority Group	RT1	RT2	RT3	RT4	RT5	RT6
1	1	2	2	2	3	1
2	1	0	4	0	5	1
3	1	0	7	6	6	1

 Table 5-4
 Damage Summary (Internal Array) for Sequence 1

Second Property Pr	0 1	2 3	4 5	6	7 8	9 10 1	1 12	13 14	15	16 17	18 19	20 21	22	23	24	25 26	27 2	18 29	30	31	32	33	34 35	36	37	38 39	40 4
Column C		t priority # damage	Ld #breach	Lb	Lexp status																				dew Thea		TotCost Pump
3 1 1 0 0 0 0 0 444 1 1 20 0 0 0 0 5 200012 0 0 0 0 1 1 0 0 0 0 0 0 0 0 0 0	8001	0 0 0	0 0				0 0	0 0	0				0 0								0.00	0.00 1	67,764 0				
\$ 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 (0 1 0	0 1				0 0	0 (0					100													
3	3 1	1 1 0	0 0			1 1 20	0 1	0 0	. 0		0 0	0	31 0	0													
3 4 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 2	2 1 0	0 0	0		1 1 21	0 1	0 0	. 0		0 0	0	31 0	0													
3 5 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 3	4 1 0	0 0) 0		1 1 22	0 1	0 (. 0		0 (0	31 0	0			0										
3 7 1 0 0 0 0 0 645	3 /	5 1 0	0 0	0			0 1	0 0	0		0 0	0	31 0	ő			ő										
3	3 F	6 1 0	0 0	0	5895	1 1 25	0 1	0 0	0	0 2001012	0 0	0	31 0	0	0.00	0.00 0	0	0.00 0.00	0	101	49.85	51.07	24,453 49	85 51.07	0.00	0.00 24,45	3 2,445,333 (
2 0 3 0 0 1 175 4752 1 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 7	7 1 0	0 0			1 1 26	0 1	0 0	0				31 0	0													
2 1 3 0 0 0 0 0 0 115 0 1 10 0 1 0 0 0 0 0 0	3 8	8 1 0	0 1			1 1 27	0 1	0 1	1	0 2001012	0 2001014	3001015	31 1														
2 2 3 0 0 0 0 573 1 1 2 0 1 0 0 0 0 0 0 0 0	2 0	0 3 0	0 1			1 1 10	0 0	0 0	. 0	0 0	0 0	0	0 1	100													
2 3 3 0 0 1 17	2	2 3 0	0 0			0 1 12	0 1	0 0		0 0	0 0	0		0													
2 4 3 0 0 0 0 0 0 0 0 0	2 1	3 3 0	0 1			1 1 13	0 1	0 1	1	0 0	0 6003074	6003075	28 1	ō			102 1										3,125,985 0
2 6 3 0 0 0 0 0 5252 0 0 1 1 55 0 1 1 0 0 0 0 0 0 0 0 0 0 0	2 /	4 3 0	0 0	0	5963	0 1 14	0 1	0 0	0	0 0	0 0	0	28 0	0	0.00		0			0						0.00	
2 7 3 0 0 0 0 0 437 0 1 177 0 1 1 77 0 1 0 0 0 0 0 0 0 0 0	2 5	5 3 0	0 0	0		0 1 15	0 1	0 0	0	0 0	0 0	0	28 0	0													, , ,
2 8 3 3 0 0 0 0 0 9699 0 1 18 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0	2 6	6 3 0	0 0			0 1 16	0 1	0 0	. 0	0 0	0 0	0	28 0	0													0 0
S	2 /	8 3 0	0 0			0 1 17	0 1	0 (. 0	0 0	0 (. 0	28 0	0) 0 0
S	5 /	0 2 0	0 1			1 1 37	0 0	0 0	. 0	0 0	0 0	0	0 1	100													3,130,453 163.3
5 2 2 0 0 0 5444 0 1 39 0 1 0 0 0 0 0 0 0 0	5	1 2 0	ō o			0 1 38	0 1	ō č	0	0 0	ō č	ő	12 0	0										00.00	0.00	0.00	
5 4 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5 2	2 2 0	0 0	0		0 1 39	0 1	0 0	0	0 0	0 0	0	12 0	0									0 0	00.00	0.00		
S S Z Q Q Q Q Q Q Q Q Q	5 ?	3 2 0	0 0				0 1	0 0	0	0 0	0 0	0	12 0	0													
5 6 2 0 0 0 0 4455 0 1 43 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5 4	4 2 0	0 0			U 1 41	0 1	0 (0	0 0	0 0	0	12 0	0													
5 7 2 0 0 0 0 588 0 1 44 0 1 0 0 0 0 0 0 0 0	5 0	6 2 0	0 0			0 1 43	0 1	0 (0 0	0 0	0	12 0	0													
7	5	7 2 0	0 0	0		0 1 44	0 1	0 0	0	0 0	0 0	0	12 0	ő						ő							0 0
7 1 2 2 0 0 0 0 5549 0 0 5 56 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5 8	8 2 0	0 0	0		0 1 45	0 1	0 0	0	0 0	0 0	0	12 0	0													
7	7 (0 2 1	800 0	0		1 0 55	0 0	0 0	0	0 0	0 0	0	0 0	100													7 31,658,667 0
7	7 1	1 2 0	0 0	0		0 0 56	0 0	0 0	0	0 0	0 0	0	32 0	0													
7 4 2 2 0 0 0 0 0 4045 0 0 99 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 2	2 2 0	0 0	0		0 0 57	0 0	0 0	. 0	0 0	0 0	0	32 0	0													
7 5 2 2 0 0 0 0 0 5544 0 0 60 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 3	4 2 0	0 0) 0		0 0 59	0 0	0 0	0	0 0	0 0	0	32 0	0) 0 0
7 7 2 0 0 0 0 4492 0 0 62 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 /	5 2 0	0 0	0	5544	0 0 60	0 0	0 0	0	0 0	0 0	0	32 0	ō			ō			ō							0 0
8 2 2 0 0 0 0 5981 0 0 83 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 €	6 2 1	800 0	0		1 0 61	1 0	0 0	0 1	1002051 0	0 0	0		101						0							
8 0 1 3 3 1125 0 0 37344 1 0 64 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 7	7 2 0	0 0	0		0 0 62	0 0	0 (0	0 0	0 0	0		0						0							
8 1 1 2 1025 0 0 3811 1 0 65 1 0 0 0 0 1001031 0 0 0 0 34 0 102 1.10 4709 322533 3 0 0.00 0.00 0.0 0 0 0.00 0.00 0.00	7 8	8 2 0	0 0	0		0 0 63	0 0	0 0	. 0	0 0	0 0	0	32 0	0													
8 2 1 1 1 100 0 0 4373 1 0 66 1 0 0 0 0 1001031 0 0 0 0 344 0 101 130 1441 31.667 0 0.00 0.00 0.00 0.00 0.00 0.00 0.0	8 .	1 1 2				1 0 65	1 0	0 (0	1001031 0	0 (0	34 0														
8 3 1 0 0 0 0 4897 0 0 67 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 7	2 1 1) 0		1 0 66	1 0	0 0			0 0	0	34 0														
8 5 1 0 0 0 0 5552 0 0 0 0 0 0 0 0 0 0 0 0 0	8 5	3 1 0	0 0	0		0 0 67	0 0	0 0	0	0 0	0 0	0	34 0	0			0			0							0 0
8 6 1 0 0 0 0 5559 0 0 70 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 4	4 1 0	0 0	0	4000	0 0 68	0 0	0 0	0	0 0	0 0	0	34 0	0													0 0
8 7 1 0 0 0 0 4410 0 0 772 0 0 71 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 5	5 1 0	0 0			0 0 69	0 0	0 0	0	0 0	0 0	0	34 0	0													0 0
8 8 1 0 0 0 0 4110 0 0 72 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 6	7 1 0	0 0			0 0 70	0 0	0 (. 0	0 0	0 0	0	34 0	0													
10	8 1	8 1 0	0 0			0 0 72	0 0	0 0	. 0	0 0	0 0	0	34 0	0													
10 2 1 1 500 1 100 4787 1 0 84 0 1 1 1 1 1 0 2001022 201023 201025 21 120 101 48.35 114.97 163.200 102 0.00 0.00 0 101 0.00 0.00 0.00		0 1 2				1 0 82	0 0	o d	0	0 0	o d	0												25 114.97	0.00		
10 3 1 0 0 0 0 4883 1 0 85 0 1 0 0 0 0 2001022 0 0 0 21 0 0 0.00 0.0	10 1	1 1 1				1 0 83	0 1	1 (0		2001023	0															
10 4 1 0 0 0 0 4413 1 0 86 0 1 0 0 0 0 2001022 0 0 0 21 0 0 0.00 0.0	10 2	2 1 1	500 1			1 0 84	0 1	1 1	. 1			3001025															16,320,000 0
10 5 1 0 0 0 0 4773 1 0 87 0 1 0 0 0 0 2001022 0 0 0 21 0 0 0 0 0 0 0 0 0	10 3	3 1 0	0 0			1 0 85	0 1	0 0	0		0 0	0		0													0 0
10 6 1 0 0 0 5488 1 0 88 0 1 0 0 0 0 0 000022 0 0 0 21 0 0 0.00 0.0		5 1 0	0 0			1 0 66	0 1	0 (0 (. 0	21 0	0													, , ,
10 7 1 0 0 0 0 4515 1 0 89 0 1 0 0 0 2001022 0 0 0 21 0 0 0.00 0.0		6 1 0	0 0	0		1 0 88	0 1	0 0	0		o d	0	21 0	0													0 0
20 0 2 1 600 2 375 40077 1 1 172 0 0 0 0 0 0 0 0 0 0 0 0 0 1 100 8551 127.66 139.94 1 100 109.79 124.66 47,520 100 0.00 0.00 0.00 0.00 0.00 0.00 0.0	10	7 1 0	0 0	0	4515	1 0 89	0 1	0 0	Ó	0 2001022	0 0	0	21 0	0			0			101	0.00					0.00	0 0
20 1 2 0 0 0 0 5999 0 1 173 0 1 0 0 0 0 0 0 16 0 0 0 0 0 0 0 0 0 0		8 1 0	0 0				0 1	0 0	0	0 2001022	0 0	0	21 0	0													
20 2 2 0 0 0 0 4337 0 1 174 0 1 0 0 0 0 0 0 16 0 0 0.00 0.00 0.00 0		0 2 1	600 2				0 0	0 0	0	0 0	0 0	0	0 1	100													
20 3 2 0 0 0 0 4317 0 1 175 0 1 0 0 0 0 0 0 0 0 16 0 0 0 0 0 0 0 0		2 0	0 0	, 0			0 1	0 (0 0	0 0	0	10 0	0													
20 4 2 0 0 1 150 5733 1 1 176 0 1 0 1 1 0 0 0 5002085 16 1 0 0.00 0.00 101 102.79 116.11 16.427 0 0.00 0.00 0.00 109.79 116.11 21.65 0.00 0.00 16.27 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		3 2 0	0 0) 0			0 1	0 (. 0	0 0	0 (0	16 0	0) 0 0
20 5 2 0 0 1 225 4156 1 1 177 0 1 0 1 1 1 0 0 0 0 5002065 16 1 0 0.00 0.00 0 101 116.11 124.66 31,093 0 0.00 0.00 0.00 0 116.11 124.66 0.00 0.00 31,093 3. 20 6 2 1 600 0 4926 1 1 178 0 1 1 0 0 0 0 4002063 0 0 16 0 101 98.51 127.66 139,947 0 0.00 0.00 0 0 0 0.00 0.00 0 98.51 127.66 0.00 0.00 189.947 13. 20 7 2 0 0 0 0 5950 0 1 179 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		4 2 0	0 1	150		1 1 176	0 1	0 1	1	0 0	0 0	5002065	16 1	0													
20 7 2 0 0 0 0 5950 0 1 179 0 1 0 0 0 0 0 0 16 0 0 0.00 0.00 0 0 0 0.00 0.0	20 5	5 2 0	0 1	225	4156	1 1 177	0 1	0 1	1	0 0	o d			0	0.00	0.00 0	101 1	16.11 124.66	31,093		0.00	0.00	0 116	11 124.66	0.00	0.00 31,09	3 3,109,333 0
		6 2 1					0 1	1 (0	0 0																	
		7 2 0					0 1	0 (0	0 0																	
20 8 2 0 0 0 0 4659 0 1 180 0 1 0 0 0 0 0 0 16 0 0 0.00 0.00 0 0 0 0.00 0.0	20 8	8 2 <u>0</u>	0 0) 0	4659	u 1 180	υ 1	0 (0	0 0	0 0	0	16 0	0	0.00	U.00 0	0	U.UO 0.00	0	0	0.00	0.00	0 0	UU 0.00	0.00	0.00	0 0

Table 5-5Sequence 1 Output

											Tend	Total		# of
Sequence									Tend		Dewater	Quantity	Total Cost	Pumps
8001									127.66		372.87	1,427,535	142,753,505	6
			# of		# of					Tstart	Tend	Total		Pump
Island	Segment	Priority	Dam	Ld	Breaches	Lb	Flooded	Tstart	Tend	Dewater	Dewater	Quantity	Total Cost	Rate
3	0	1	0	0	1	300	1	1.50	98.41	98.41	154.17	224,340	22,433,956	56.47
2	0	3	0	0	1	175	1	115.17	130.42	130.42	263.93	31,260	3,125,985	56.47
5	0	2	0	0	1	250	1	98.61	109.79	109.79	208.64	31,305	3,130,453	163.35
7	0	2	1	800	0	0	0	1.40	92.17	0.00	0.00	316,587	31,658,667	0.00
8	0	1	3	1125	0	0	0	1.10	47.09	0.00	0.00	354,000	35,400,000	0.00
10	0	1	2	925	1	100	0	46.25	114.97	0.00	0.00	282,578	28,257,778	0.00
20	0	2	1	600	2	375	1	98.51	127.66	127.66	372.87	187,467	18,746,667	56.47

Table 5-6 Output to Water Quality Model for Sequence 1

Sequence]										
8001					Tstart	Tend	Tstart	Tend			
		# Of			Breach	Breach	All	All	Tstart	Tend	Pump
Island	Segment	Breaches	Lb	Tbreach	Repair	Repair	Repairs	Repairs	Dewater	Dewater	Rate
3	0	1	300	1	46.15	98.41	1.50	98.41	98.41	154.17	56.47
3	1	0	0	0	0.00	0.00	1.50	2.45	0.00	0.00	0.00
3	2	0	0	0	0.00	0.00	45.45	46.47	0.00	0.00	0.00
3	3	0	0	0	0.00	0.00	46.47	47.55	0.00	0.00	0.00
3	4	0	0	0	0.00	0.00	47.55	48.77	0.00	0.00	0.00
3	5	0	0	0	0.00	0.00	48.77	49.85	0.00	0.00	0.00
3	6	0	0	0	0.00	0.00	49.85	51.07	0.00	0.00	0.00
3	7	0	0	0	0.00	0.00	51.07	52.04	0.00	0.00	0.00
3	8	1	300	1	46.15	98.41	46.15	98.41	0.00	0.00	0.00
2	0	1	175	1	115.17	130.42	115.17	130.42	130.42	263.93	56.47
2	1	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	2	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	3	1	175	1	115.17	130.42	115.17	130.42	0.00	0.00	0.00
2	4	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	5	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	6	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	7	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	8	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0	1	250	1	98.61	109.79	98.61	109.79	109.79	208.64	163.35
5	1	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	2	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	3	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	4	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	5	1	250	1	98.61	109.79	98.61	109.79	0.00	0.00	0.00
5	6	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	7	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	8	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	0	2	375	1	109.79	124.66	98.51	127.66	127.66	372.87	56.47
20	1	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	2	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	3	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	4	1	150	1	109.79	116.11	109.79	116.11	0.00	0.00	0.00
20	5	1	225	1	116.11	124.66	116.11	124.66	0.00	0.00	0.00
20	6	0	0	0	0.00	0.00	98.51	127.66	0.00	0.00	0.00
20	7	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	8	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00

5.2 Sequence 2

The second sample sequence (sequence # 8002) involves 10 impacted islands. Each island has experienced a single breach that occurs on Day 1. The islands belong to the same island priority group. Tables 5-7 through 5-9 present the input (damage, assignment to island priority groups, and repair work order prioritization for each island priority group). Table 5-10 presents the internal Damage Summary array, which keeps track of the repairs and their priorities. The main ER&R model output is presented in Table 5-11 and the output that is passed on to the Water Quality model is presented in Table 5-12.

Table 5-7 Sequence 2 Damage Input

Sequence Id	Day Of Year				
8002	180				
		Damage	Length	Slump Height /Breach Growth Rate	Time
Island Id	Segment	State	(Feet)	(Inches)	(Days)
1	8	2	300	4	1
25	4	2	250	4	1
9	5	2	175	4	1
3	2	2	375	4	1
30	2	2	350	4	1
8	1	2	200	4	1
44	6	2	300	4	1
43	5	2	425	4	1
10	7	2	375	4	1
11	2	2	275	4	1

 Table 5-8
 Sequence 2 Island Priority Group Input

Sequence Id	
8002	
	Island
T-1 1 T-1	Priority
Island Id	Group
1	1
25	1
9	1
3	1
30	1
8	1
44	1
43	1
10	1
11	1

 Table 5-9
 Sequence 2 Repair Order Prioritization Input

Sequence						
Id						
8002						
Island Priority						
Priority Group	RT1	RT2	RT3	RT4	RT5	RT6
					2120	
1	1	2	2	2	3	1
1 2	1 1	2	2 4	2 0	3 5	1 1

 Table 5-10
 Damage Summary (Internal Array) for Sequence 2

43 43 43 43 43 43 43 43 10 10 10 10 10 10 10 11 11 11	8 8 8 8 8 8 44 44 44 44 44 44 44	3 3 3 30 30 30 30 30 30 30 30 30 30 30 3	9 9 9 9 9 9 3 3 3 3	25 25 25 25 25 25 25 25 25 25 25 25 25 2	8002 1 1 1 1 1 1 1 1
0 1 2 3 4 5 6 7 8 0 1 2 3 4 5 6 7 8 0 0 1 2 3 4 5 6 7 8 0 0 1 1 2 3 4 5 6 6 7 8 0 1 8 0 1 8 0 1 1 1 1 1 1 1 1 1 1 1 1	2 3 4 5 6 7 8 0 1 2 3 4 5 6 7 8	6 7 8 0 1 2 3 4 5 6 7 8 0	2 3 4 5 6 7 8 0 1 2 3 4	0 1 2 3 4 5 6 7 8 0	ment priority 0 0 1 2 3 4 5 6 7
1 0 1 1 0 1 1 1 1 0 1 1 1 1 1 0 1 1 1 1 1 0 1	1 0 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0	1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	# damage Ld 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1
0 0 0 44 0 0 0 0 55 0 1 425 33 0 0 0 55 0 0 0 0	0 0 0 44 0 0 0 0 55 0 0 0 0 55 0 0 0 0 56 0 0 0 0 56 0 0 0 0 56 0 0 0 0 44 0 0 0 0 55 0 0 0 0 55 0 0 0 0 55 0 0 0 0	0 0 0 44 0 0 0 0 44 0 1 350 37 0 1 350 37 0 0 0 0 44 0 0 0 0 44 0 0 0 5 0 0 0 0 44 0 0 0 44 0 0 0 44 0 0 0 44 0 0 0 38 0 0 0 5 0 0 0 38	0 0 0 55 0 0 0 44 0 1 175 56 0 0 0 56 0 0 0 56 0 1 375 40 0 1 375 40 0 1 375 40 0 0 0 56	1 250 418 0 0 0 418 0 0 0 58 0 1 250 448 0 0 0 418 0 0 0 448 0 0 0 58 0 0 0 58 0 0 0 58 0 0 0 58 0 0 0 0 58 0 0 0 0 58 0 0 0 0 58	0 0 0 50 0 0 0 55 0 0 0 55 0 0 0 45 0 0 0 55 0 0 0 45
313 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	471 1 1 528 1 1 2555 1 325 1 1 223 1 785 1 730 1 1 563 1 1 562 1 1	586 1 588 1 579 1 350 1 776 1 553 1 327 1 217 1 269 1	366 1 781 1 1446 1 161 1 1515 1 1525 1 16368 1 1604 1 1559 1 1600 1 1777 1 17877 1 1796 1	906 1 990 1 1507 1 1771 1 885 1 1559 1 1555 1 959 1 1580 1 1433 1	0 0
1 379 0 0 1 389 0 0 1 389 0 0 1 384 0 0 1 384 0 0 1 384 0 0 1 385 0 0 1 385 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 88 0 0 1 90 0 0 1 90 0 0 1 90 0 0 1 90 0 0 1 90 0 0 0	1 66 0 1 67 0 1 68 0 1 69 0 1 71 0 1 71 0 1 72 0 1 389 0 1 390 0 1 391 0 1 393 0 1 394 0 1 395 0	1 25 0 1 26 0 1 27 0 1 282 0 1 282 0 1 283 0 1 284 0 1 285 0 1 286 0 1 286 0 1 288 0 1 288 0 1 270 0 1 64 0	1 75 0 1 76 0 1 77 0 1 78 0 1 79 0 1 80 0 1 81 0 1 19 0 1 20 0 1 21 0 1 22 0	1 217 0 1 218 0 1 219 0 1 220 0 1 221 0 1 222 0 1 222 0 1 223 0 1 224 0 1 225 0 1 73 0	0 0 0 0 0 0 1 1 1 2 0 0 1 1 5 0 0 1 1 5 0 0 1 1 6 0 0 1 1 7 0 0 1 1 8 0 0 1 1 1 8 0 0 1 1 1 8 0 0 1 1 1 8 0 0 1 1 1 8 0 0 1 1 1 8 0 0 1 1 1 8 0 0 1 1 1 1
0 0 1 0 1 0 1 0 1 0 1 0 0 1 1	1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	1 0 1 0 1 0 0 0 1 0 1 0 1 0 1 0 1 0 1 0	1 0 1 0 1 0 1 0 1 0 1 0 1 0 0 0 0 0 1 0 1	0 0 1 0 1 0 1 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0	12 13 14 RT2 RT3 RT4 0 0 0 1 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0
		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT5 PRT
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0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
0 34 0 34 0 34 0 0 0 21 0 21 0 21 0 21 0 21	0 34 0 34 0 34 0 34 0 34 0 34 0 34 0 0 0 0 38 0 38 0 38 0 38 0 38 0 38 0 3	0 18 0 18 0 18 0 18 0 18 0 18 0 18 0 31	0 38 0 38 0 38 0 0 0 31	0 0 10 0 10 0 10 0 10 0 10 0 10 0 10 0	20 21 22 T5 ow(MHHW) Tbreach 0 0 0 0 24 0 24 0 24 0 24 0 24 0 24 0 24 0 24 0 24
100	0 0 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0 0 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0 0 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0 100 0.00 0.00 0 0 0.00 0.00 0 0 0.00 0.0	23 24 25 1 26 1 27 28 1 28 1 28 1 28 1 28 1 28 1 28 1
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 100 0 0 0 0 0 102 0 0 0 0 0 0 0 0 0 0	nVol brstat brT 0 0 100 0 100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
8.95 80.27 87,544 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0 0.00 0.00 0 0.00 0.00 0 0.355 54.64 54.613 0.00 0.00 0 0.00 0.00 0 0.00 0.00 0 0.00 0.00	0.00 0.00 0 0.00 0.00 0 0.00 0.00 0 1.90 1.87 31,659 0.00 0.00 0 0.00 0.00 0 0.00 0.00 0 5.13 62.68 72,292 0.00 0.00 0 0.00 0.00 0 0.00 0.00 0 0.00 0.00	6.21 31.57 39,328 0.00 0.00 0 0.00 0.00 0 0.00 0.00 0 0.00 0.00	
101 75.11 76.21 22.03 101 77.24 77.30 17.00 101 77.24 78.00 17.00 101 77.24 78.00 17.00 101 79.97 80.88 20.88 101 89.98 82.11 22.88 101 82.11 80.88 20.88 20.88 101 80.98 82.11 22.88 101 80.98 82.11 22.88 102 82.88 103 82.88 104 82.88 105 82.88 107 82.88 108	101 13.80 14.87 23.47 101 14.97 16.14 23.47 101 16.14 16.99 16.89 101 16.99 17.84 17.84 100 42.94 50.92 159.85 101 44.09 45.18 21.79 101 44.09 45.18 21.79 101 47.14 48.13 19.84 101 47.14 48.13 19.84 101 49.95 16.87 101 49.95 16.95	101 64.07 65.30 24.45.3 101 68.27 67.17 18.09 100 508.27 67.17 18.09 101 68.27 67.17 18.09 101 51.89 52.70 18.12 101 52.89 52.70 18.12 101 52.70 53.67 18.12 101 52.70 53.67 18.12 101 52.77 53.67 18.12 101 52.77 53.67 21.88 101 58.77 57.27 20.02 101 59.97 57.70 20.02 101 59.90 17.84 18.12 101 99.90 17.84 18.12 101 101 99.90 17.84 18.12	101 4.55 5.52 19.27: 101 5.52 6.56 20.99 101 6.56 7.79 24.53 101 7.79 8.85 21.255 101 8.85 9.90 20.22: 100 58.80 67.7 197.45 101 58.80 59.75 19.08 101 59.75 60.70 18.91 101 60.70 61.78 21.57 101 61.78 63.00 24.37	100	31 32 33 34 crosstat erosTest erosTend erosVol 0 000 000 1643,846 100 34.44 42.94 17.00 101 34.44 32.94 17.00 101 36.52 37.62 21,97 101 36.52 37.62 21,97 101 38.76 39.75 19,70 101 40.94 41.81 17.50 101 40.94 41.81 17.50 101 41.81 42.94 22.64
75.11 76.21 0.00 0.00 22.039 2.203.911 76.21 77.24 0.00 0.00 20.53 2.053.33 77.24 76.09 0.00 0.00 1.00 17.003 1.700.326 78.09 79.20 0.00 0.00 12.259 2.225.896 18.80 80.27 0.00 0.00 1.00 12.259 2.225.896 18.80 80.27 0.00 0.00 1.00 10.265 10.286.636 18.80 80.27 0.00 0.00 1.00 10.265 10.286.636 18.81 0.00 0.00 10.255 10.286.636 18.81 0.00 0.00 22.57 2.258.687 18.21 0.00 0.00 22.57 2.258.687 17.17 88.04 0.00 0.00 22.719 2.271.911 17.12 75.11 75.11 84.13 22.7794.277,9413 17.13 71.05 0.00 0.00 17.435 1.743.467 18.14 1.00 0.00 1.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787 17.10 77.10 0.00 0.00 18.205 1.825.787	118.7 12.79 0.00 0.00 18.239 1.823.941 0 12.79 13.80 0.00 0.00 22.23 2.024.268 0 13.80 14497 0.00 0.00 22.3404 2.340,385 0 14.897 0.00 0.00 23.404 2.340,385 0 16.99 17.84 0.00 0.00 15.89 11.89,389 0 16.99 17.84 0.00 0.00 17.049 1.704.89 0 16.99 17.84 0.00 0.00 17.049 1.704.89 0 16.99 17.84 0.00 0.00 12.331 2.293,096 0 18.29 18.2	64.07 65.30 0.00 0.00 24.453 2.445.33 0 65.30 66.27 0.00 0.00 19.393 1.993.259 0 66.27 67.17 0.00 0.00 19.393 1.993.259 0 66.27 67.17 0.00 0.00 19.393 1.993.259 0 67.35 212.142.27 56.45 0 67.35 212.142.27 56.25 212.142.27 56.25 212.142.27 56.25 212.142.27 56.25 212.142.27 56.25 212.142.27 56.25	33.5 4.55 0.00 0.00 23.890 2.389.04 0	6.21 31.57 31.57 147.02 213.160 21.316.07 377.726 17.84 18.85 0.00 0.00 20.284 2.028,444 0.01 18.85 19.99 0.00 0.00 19.781 1.1979.081 0.00 6.21 31.57 0.00 1.00 19.781 1.1979.081 0.00 1.00 19.781 1.1979.081 0.00 1.00 19.781 1.207.087 1.00 1.00 10.00 19.781 1.207.087 1.00 1.00 10.00 10.00 19.781 1.207.087 1.00 1.00 10.	9.39 42.94 42.94 137.54 225,736 22.573.60 377.126 35.47 36.52 0.00 0.00 20,732 2,073.244 0.00 35.52 37.52 0.00 0.00 21,972 2,092.328 0 35.52 37.52 0.00 0.00 21,972 2,197.808 0.00 38.76 38.75 0.00 0.00 18,704 1,970.370 0 38.76 38.75 0.00 0.00 18,704 1,970.370 0

 Table 5-11
 Sequence 2 Output

											Tend	Total		# of
Sequence									Tend		Dewater	Quantity	Total Cost	Pumps
8002									58.80		257.35	2,196,028	219,602,756	57
			# of		# of					Tstart	Tend	Total		Pump
Island	Segment	Priority	Dam	Ld	Breaches	Lb	Flooded	Tstart	Tend	Dewater	Dewater	Quantity	Total Cost	Rate
1	8	1	0	0	1	300	1	9.39	42.94	42.94	137.54	225,736	22,573,600	377.13
25	4	1	0	0	1	250	1	6.21	31.57	31.57	147.02	213,160	21,316,047	377.13
9	5	1	0	0	1	175	1	1.10	15.87	15.87	164.80	207,677	20,767,704	56.47
3	2	1	0	0	1	375	1	15.13	67.17	67.17	122.94	239,744	23,974,400	56.47
30	2	1	0	0	1	350	1	13.55	58.80	58.80	257.35	212,143	21,214,287	56.47
8	1	1	0	0	1	200	1	4.04	23.38	23.38	236.07	197,450	19,745,007	56.47
44	6	1	0	0	1	300	1	11.29	50.92	50.92	149.58	222,071	22,207,111	590.90
43	5	1	0	0	1	425	1	18.96	83.29	83.29	98.62	251,196	25,119,644	56.47
10	7	1	0	0	1	375	1	17.12	75.11	75.11	84.13	227,794	22,779,413	56.47
11	2	1	0	0	1	275	1	7.85	35.91	35.91	125.20	199,055	19,905,541	56.47

 Table 5-12
 Output to Water Quality Model for Sequence 2

Sequence											
8002											
Island	Segment	# of Breaches	Lb	Tbreach	Tstart Breach Repair	Tend Breach Repair	Tstart All Repairs	Tend All Repairs	Tstart Dewater	Tend Dewater	Pump Rate
1	0	1	300	1	9.39	41.92	9.39	42.94	42.94	137.54	377.13
1	1	0	0	0	0.00	0.00	34.44	35.47	0.00	0.00	0.00
1	2	0	0	0	0.00	0.00	35.47	36.52	0.00	0.00	0.00
1	3	0	0	0	0.00	0.00	36.52	37.62	0.00	0.00	0.00
1	4	0	0	0	0.00	0.00	37.62	38.76	0.00	0.00	0.00
1	5	0	0	0	0.00	0.00	38.76	39.75	0.00	0.00	0.00
1	6	0	0	0	0.00	0.00	39.75	40.94	0.00	0.00	0.00
1	7	0	0	0	0.00	0.00	40.94	41.81	0.00	0.00	0.00
1	8	1	300	1	9.39	41.92	9.39	42.94	0.00	0.00	0.00
25	0	1	250	1	6.21	31.57	6.21	31.57	31.57	147.02	377.13
25	1	0	0	0	0.00	0.00	17.84	18.85	0.00	0.00	0.00
25	2	0	0	0	0.00	0.00	18.85	19.99	0.00	0.00	0.00
25	3	0	0	0	0.00	0.00	19.99	20.98	0.00	0.00	0.00
25	4	1	250	1	6.21	31.57	6.21	31.57	0.00	0.00	0.00
25	5	0	0	0	0.00	0.00	22.00	23.03	0.00	0.00	0.00
25	6	0	0	0	0.00	0.00	23.03	24.14	0.00	0.00	0.00
25	7	0	0	0	0.00	0.00	24.14	25.37	0.00	0.00	0.00
25	8	0	0	0	0.00	0.00	25.37	26.53	0.00	0.00	0.00
9	0	1	175	1	1.90	15.87	1.10	15.87	15.87	164.80	56.47
9	1	0	0	0	0.00	0.00	1.10	2.24	0.00	0.00	0.00
9	2	0	0	0	0.00	0.00	2.24	3.35	0.00	0.00	0.00
9	3	0	0	0	0.00	0.00	3.35	4.55	0.00	0.00	0.00
9	4	0	0	0	0.00	0.00	4.55	5.52	0.00	0.00	0.00
9	5	1	175	1	1.90	15.87	1.90	15.87	0.00	0.00	0.00
9	6	0	0	0	0.00	0.00	6.56	7.79	0.00	0.00	0.00
9	7	0	0	0	0.00	0.00	7.79	8.85	0.00	0.00	0.00
9	8	0	0	0	0.00	0.00	8.85	9.90	0.00	0.00	0.00
3	0	1	375	1	15.13	62.68	15.13	67.17	67.17	122.94	56.47
3	1	0	0	0	0.00	0.00	58.80	59.75	0.00	0.00	0.00
3	2	1	375	1	15.13	62.68	15.13	62.68	0.00	0.00	0.00
3	3	0	0	0	0.00	0.00	60.70	61.78	0.00	0.00	0.00
3	4	0	0	0	0.00	0.00	61.78	63.00	0.00	0.00	0.00
3	5	0	0	0	0.00	0.00	63.00	64.07	0.00	0.00	0.00
3	6	0	0	0	0.00	0.00	64.07	65.30	0.00	0.00	0.00
3	7	0	0	0	0.00	0.00	65.30	66.27	0.00	0.00	0.00
3	8	0	0	0	0.00	0.00	66.27	67.17	0.00	0.00	0.00
30	0	1	350	1	13.55	54.64	13.55	58.80	58.80	257.35	56.47
30	1	0	0	0	0.00	0.00	50.92	51.89	0.00	0.00	0.00
30	2	1	350	1	13.55	54.64	13.55	54.64	0.00	0.00	0.00
30	3	0	0	0	0.00	0.00	52.70	53.67	0.00	0.00	0.00
30	4	0	0	0	0.00	0.00	53.67	54.78	0.00	0.00	0.00
30	5	0	0	0	0.00	0.00	54.78	55.77	0.00	0.00	0.00
30	6	0	0	0	0.00	0.00	55.77	56.72	0.00	0.00	0.00
30	7	0	0	0	0.00	0.00	56.72	57.72	0.00	0.00	0.00
30	8	0	0	0	0.00	0.00	57.72	58.80	0.00	0.00	0.00
8	0	1	200	1	4.04	23.38	4.04	23.38	23.38	236.07	56.47
8	1	1	200	1	4.04	23.38	4.04	23.38	0.00	0.00	0.00
8	2	0	0	0	0.00	0.00	10.86	11.87	0.00	0.00	0.00
8	3	0	0	0	0.00	0.00	11.87	12.79	0.00	0.00	0.00
8	4	0	0	0	0.00	0.00	12.79	13.80	0.00	0.00	0.00
8	5	0	0	0	0.00	0.00	13.80	14.97	0.00	0.00	0.00

Table 5-12 Output to Water Quality Model for Sequence 2

Sequence]										
8002											
					Tstart	Tend	Tstart	Tend			
		# of			Breach	Breach	All	All	Tstart	Tend	Pump
Island	Segment	Breaches	Lb	Tbreach	Repair	Repair	Repairs	Repairs	Dewater	Dewater	Rate
8	6	0	0	0	0.00	0.00	14.97	16.14	0.00	0.00	0.00
8	7	0	0	0	0.00	0.00	16.14	16.99	0.00	0.00	0.00
8	8	0	0	0	0.00	0.00	16.99	17.84	0.00	0.00	0.00
44	0	1	300	1	11.29	48.60	11.29	50.92	50.92	149.58	590.90
44	1	0	0	0	0.00	0.00	42.94	44.09	0.00	0.00	0.00
44	2	0	0	0	0.00	0.00	44.09	45.18	0.00	0.00	0.00
44	3	0	0	0	0.00	0.00	45.18	46.08	0.00	0.00	0.00
44	4	0	0	0	0.00	0.00	46.08	47.14	0.00	0.00	0.00
44	5	0	0	0	0.00	0.00	47.14	48.13	0.00	0.00	0.00
44	6	1	300	1	11.29	48.60	11.29	49.11	0.00	0.00	0.00
44	7	0	0	0	0.00	0.00	49.11	49.95	0.00	0.00	0.00
44	8	0	0	0	0.00	0.00	49.95	50.92	0.00	0.00	0.00
43	0	1	425	1	18.96	80.27	18.96	83.29	83.29	98.62	56.47
43	1	0	0	0	0.00	0.00	75.11	76.21	0.00	0.00	0.00
43	2	0	0	0	0.00	0.00	76.21	77.24	0.00	0.00	0.00
43	3	0	0	0	0.00	0.00	77.24	78.09	0.00	0.00	0.00
43	4	0	0	0	0.00	0.00	78.09	79.20	0.00	0.00	0.00
43	5	1	425	1	18.96	80.27	18.96	80.27	0.00	0.00	0.00
43	6	0	0	0	0.00	0.00	79.97	80.98	0.00	0.00	0.00
43	7	0	0	0	0.00	0.00	80.98	82.11	0.00	0.00	0.00
43	8	0	0	0	0.00	0.00	82.11	83.29	0.00	0.00	0.00
10	0	1	375	1	17.12	70.38	17.12	75.11	75.11	84.13	56.47
10	1	0	0	0	0.00	0.00	67.17	68.04	0.00	0.00	0.00
10	2	0	0	0	0.00	0.00	68.04	69.16	0.00	0.00	0.00
10	3	0	0	0	0.00	0.00	69.16	70.13	0.00	0.00	0.00
10	4	0	0	0	0.00	0.00	70.13	71.05	0.00	0.00	0.00
10	5	0	0	0	0.00	0.00	71.05	72.04	0.00	0.00	0.00
10	6	0	0	0	0.00	0.00	72.04	73.18	0.00	0.00	0.00
10	7	1	375	1	17.12	70.38	17.12	74.04	0.00	0.00	0.00
10	8	0	0	0	0.00	0.00	74.04	75.11	0.00	0.00	0.00
11	0	1	275	1	7.85	35.91	7.85	35.91	35.91	125.20	56.47
11	1	0	0	0	0.00	0.00	26.53	27.69	0.00	0.00	0.00
11	2	1	275	1	7.85	35.91	7.85	35.91	0.00	0.00	0.00
11	3	0	0	0	0.00	0.00	28.61	29.51	0.00	0.00	0.00
11	4	0	0	0	0.00	0.00	29.51	30.35	0.00	0.00	0.00
11	5	0	0	0	0.00	0.00	30.35	31.34	0.00	0.00	0.00
11	6	0	0	0	0.00	0.00	31.34	32.21	0.00	0.00	0.00
11	7	0	0	0	0.00	0.00	32.21	33.33	0.00	0.00	0.00
11	8	0	0	0	0.00	0.00	33.33	34.44	0.00	0.00	0.00

5.3 Sequential Output in Text File Format

The main ER&R output will be output sequentially to a text file for all sequences analyzed. Each sequence will start with the sequence ID. Sequence completion will be delineated by a line starting with -99999. The output from the ER&R model to the water quality model will similarly be output to a text file, which will include a large set of sequences, each identified by its sequence ID and ended by a line starting with -99999.

Figures 5-1 and 5-2 present the appearance of these two text files for the case of two example sequences. Figure 5-1 presents the text file that includes the output that was presented in Tables 5-5 and 5-11 for sequences 8001 and 8002, respectively. The column headings are not shown on Figure 5-1, as these do not appear in the sequential text file, but they are identical to the headers in Tables 5-5 and 5-11. Figure 5-2 presents the text file that includes the output that was presented in Tables 5-6 and 5-12 for the two sequences analyzed. The column headings are not shown on Figure 5-2, as these do not appear in the sequential text file, but they are identical to the headers in Tables 5-6 and 5-12.



Figure 5-1 Appearance of Sequential Outputs (for 2 Sequences)

8001	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	127.66	0	372.87	1,427,535	142,753,505	6
3	0	1	0	0	1	300	1	1.50	98.41	98.41	154.17	224,340	22,433,956	56.47
2	0	3	0	0	1	175	1	115.17	130.42	130.42	263.93	31,260	3,125,985	56.47
5	0	2	0	0	1	250	1	98.61	109.79	109.79	208.64	31,305	3,130,453	163.35
7	0	2	1	800	0	0	0	1.40	92.17	0.00	0.00	316,587	31,658,667	0.00
8	0	1	3	1125	0	0	0	1.10	47.09	0.00	0.00	354,000	35,400,000	0.00
10	0	1	2	925	1	100	0	46.25	114.97	0.00	0.00	282,578	28,257,778	0.00
20	0	2	1	600	2	375	1	98.51	127.66	127.66	372.87	187,467	18,746,667	56.47
-99999	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8002	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	58.80	0	257.35	2,196,028	219,602,756	57
1	8	1	0	0	1	300	1	9.39	42.94	42.94	137.54	225,736	22,573,600	377.13
25	4	1	0	0	1	250	1	6.21	31.57	31.57	147.02	213,160	21,316,047	377.13
9	5	1	0	0	1	175	1	1.10	15.87	15.87	164.80	207,677	20,767,704	56.47
3	2	1	0	0	1	375	1	15.13	67.17	67.17	122.94	239,744	23,974,400	56.47
30	2	1	0	0	1	350	1	13.55	58.80	58.80	257.35	212,143	21,214,287	56.47
8	1	1	0	0	1	200	1	4.04	23.38	23.38	236.07	197,450	19,745,007	56.47
44	6	1	0	0	1	300	1	11.29	50.92	50.92	149.58	222,071	22,207,111	590.90
43	5	1	0	0	1	425	1	18.96	83.29	83.29	98.62	251,196	25,119,644	56.47
10	7	1	0	0	1	375	1	17.12	75.11	75.11	84.13	227,794	22,779,413	56.47
11	2	1	0	0	1	275	1	7.85	35.91	35.91	125.20	199,055	19,905,541	56.47
-99999	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Figure 5-2 Appearance of Sequential Outputs to Water Quality Module (for 2 Sequences)

	0	0	0	0	0	0	0	0	0	0	0
3	0	1	300	1	46.15	98.41	1.50	98.41	98.41	154.17	56.47
3	1	0	0	0	0.00	0.00	1.50	2.45	0.00	0.00	0.00
3	2	0	0	0	0.00	0.00	45.45	46.47	0.00	0.00	0.00
3	3	0	0	0	0.00	0.00	46.47	47.55	0.00	0.00	0.00
3	4	0	0	0	0.00	0.00	47.55	48.77	0.00	0.00	0.00
3	5	0	0	0	0.00	0.00	48.77	49.85	0.00	0.00	0.00
3	6	0	0	0	0.00	0.00	49.85	51.07	0.00	0.00	0.00
3	7	0	0	0	0.00	0.00	51.07	52.04	0.00	0.00	0.00
3	8	1	300	1	46.15	98.41	46.15	98.41	0.00	0.00	0.00
2	0	1	175	1	115.17	130.42	115.17	130.42	130.42	263.93	56.47
2	1	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	2	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	3	1	175	1	115.17	130.42	115.17	130.42	0.00	0.00	0.00
2	4	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	5	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	6	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	7	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	8	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0	1	250	1	98.61	109.79	98.61	109.79	109.79	208.64	163.35
5	1	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	2	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	3	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	4	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	5	1	250	1	98.61	109.79	98.61	109.79	0.00	0.00	0.00
5	6	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	7	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	8	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	0	2	375	1	109.79	124.66	98.51	127.66	127.66	372.87	56.47
20	1	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	2	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	3	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	4	1	150	1	109.79	116.11	109.79	116.11	0.00	0.00	0.00
20	5	1	225	1	116.11	124.66	116.11	124.66	0.00	0.00	0.00
20	6	0	0	0	0.00	0.00	98.51	127.66	0.00	0.00	0.00
20	7	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	8	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-99999	0	0	0	0	0	0	0	0	0	0	0
8002	0	0	0	0	0	0	0	0	0	0	0
1	0	1	300	1	9.39	41.92	9.39	42.94	42.94	137.54	377.13
1	1	0	0	0	0.00	0.00	34.44	35.47	0.00	0.00	0.00
1	2	0	0	0	0.00	0.00	35.47	36.52	0.00	0.00	0.00
1	3	0	0	0	0.00	0.00	36.52	37.62	0.00	0.00	0.00
1	4	0	0	0	0.00	0.00	37.62	38.76	0.00	0.00	0.00
1	5	0	0	0	0.00	0.00	38.76	39.75	0.00	0.00	0.00
1	6	0	0	0	0.00	0.00	39.75	40.94	0.00	0.00	0.00
1	7	0	0	0	0.00	0.00	40.94	41.81	0.00	0.00	0.00
1	8	1	300	1	9.39	41.92	9.39	42.94	0.00	0.00	0.00
25	0	1	250	1	6.21	31.57	6.21	31.57	31.57	147.02	377.13

Figure 5-2 Appearance of Sequential Outputs to Water Quality Module (for 2 Sequences)

25	1	0	0	0	0.00	0.00	17.84	18.85	0.00	0.00	0.00
25	2	0	0	0	0.00	0.00	18.85	19.99	0.00	0.00	0.00
25	3	0	0	0	0.00	0.00	19.99	20.98	0.00	0.00	0.00
25	4	1	250	1	6.21	31.57	6.21	31.57	0.00	0.00	0.00
25	5	0	0	0	0.00	0.00	22.00	23.03	0.00	0.00	0.00
25	6	0	0	0	0.00	0.00	23.03	24.14	0.00	0.00	0.00
25	7	0	0	0	0.00	0.00	24.14	25.37	0.00	0.00	0.00
25	8	0	0	0	0.00	0.00	25.37	26.53	0.00	0.00	0.00
9	0	1	175	1	1.90	15.87	1.10	15.87	15.87	164.80	56.47
9	1	0	0	0	0.00	0.00	1.10	2.24	0.00	0.00	0.00
9	2	0	0	0	0.00	0.00	2.24	3.35	0.00	0.00	0.00
9	3	0	0	0	0.00	0.00	3.35	4.55	0.00	0.00	0.00
9	4	0	0	0	0.00	0.00	4.55	5.52	0.00	0.00	0.00
9	5	1	175	1	1.90	15.87	1.90	15.87	0.00	0.00	0.00
9	6	0	0	0	0.00	0.00	6.56	7.79	0.00	0.00	0.00
9	7	0	0	0	0.00	0.00	7.79	8.85	0.00	0.00	0.00
9	8	0	0	0	0.00	0.00	8.85	9.90	0.00	0.00	0.00
3	0	1	375	1	15.13	62.68	15.13	67.17	67.17	122.94	56.47
3	1	0	0	0	0.00	0.00	58.80	59.75	0.00	0.00	0.00
3	2	1	375	1	15.13	62.68	15.13	62.68	0.00	0.00	0.00
3	3	0	0	0	0.00	0.00	60.70	61.78	0.00	0.00	0.00
3	4	0	0	0	0.00	0.00	61.78	63.00	0.00	0.00	0.00
3	5	0	0	0	0.00	0.00	63.00	64.07	0.00	0.00	0.00
3	6	0	0	0	0.00	0.00	64.07	65.30	0.00	0.00	0.00
3	7	0	0	0	0.00	0.00	65.30	66.27	0.00	0.00	0.00
3	8	0	0	0	0.00	0.00	66.27	67.17	0.00	0.00	0.00
30	0	1	350	1	13.55	54.64	13.55	58.80	58.80	257.35	56.47
30	1	0	0	0	0.00	0.00	50.92	51.89	0.00	0.00	0.00
30	2	1	350	1	13.55	54.64	13.55	54.64	0.00	0.00	0.00
30	3	0	0	0	0.00	0.00	52.70	53.67	0.00	0.00	0.00
30	4	0	0	0	0.00	0.00	53.67	54.78	0.00	0.00	0.00
30	5	0	0	0	0.00	0.00	54.78	55.77	0.00	0.00	0.00
30	6	0	0	0	0.00	0.00	55.77	56.72	0.00	0.00	0.00
30	7	0	0	0	0.00	0.00	56.72	57.72	0.00	0.00	0.00
30	8	0	0	0	0.00	0.00	57.72	58.80	0.00	0.00	0.00
8	0	1	200	1	4.04	23.38	4.04	23.38	23.38	236.07	56.47
8	1	1	200	1	4.04	23.38	4.04	23.38	0.00	0.00	0.00
8	2	0	0	0	0.00	0.00	10.86	11.87	0.00	0.00	0.00
8	3	0	0	0	0.00	0.00	11.87	12.79	0.00	0.00	0.00
8	4	0	0	0	0.00	0.00	12.79	13.80	0.00	0.00	0.00
8	5	0	0	0	0.00	0.00	13.80	14.97	0.00	0.00	0.00
8	6	0	0	0	0.00	0.00	14.97	16.14	0.00	0.00	0.00
8	7	0	0	0	0.00	0.00	16.14	16.99	0.00	0.00	0.00
8	8	0	0	0	0.00	0.00	16.99	17.84	0.00	0.00	0.00
44	0	1	300	1	11.29	48.60	11.29	50.92	50.92	149.58	590.90
44	1	0	0	0	0.00	0.00	42.94	44.09	0.00	0.00	0.00
44	2	0	0	0	0.00	0.00	44.09	45.18	0.00	0.00	0.00
44	3	0	0	0	0.00	0.00	45.18	46.08	0.00	0.00	0.00
44	4	0	0	0	0.00	0.00	46.08	47.14	0.00	0.00	0.00
44	5	0	0	0	0.00	0.00	47.14	48.13	0.00	0.00	0.00

Figure 5-2 Appearance of Sequential Outputs to Water Quality Module (for 2 Sequences)

44	6	1	300	1	11.29	48.60	11.29	49.11	0.00	0.00	0.00
44	7	0	0	0	0.00	0.00	49.11	49.95	0.00	0.00	0.00
44	8	0	0	0	0.00	0.00	49.95	50.92	0.00	0.00	0.00
43	0	1	425	1	18.96	80.27	18.96	83.29	83.29	98.62	56.47
43	1	0	0	0	0.00	0.00	75.11	76.21	0.00	0.00	0.00
43	2	0	0	0	0.00	0.00	76.21	77.24	0.00	0.00	0.00
43	3	0	0	0	0.00	0.00	77.24	78.09	0.00	0.00	0.00
43	4	0	0	0	0.00	0.00	78.09	79.20	0.00	0.00	0.00
43	5	1	425	1	18.96	80.27	18.96	80.27	0.00	0.00	0.00
43	6	0	0	0	0.00	0.00	79.97	80.98	0.00	0.00	0.00
43	7	0	0	0	0.00	0.00	80.98	82.11	0.00	0.00	0.00
43	8	0	0	0	0.00	0.00	82.11	83.29	0.00	0.00	0.00
10	0	1	375	1	17.12	70.38	17.12	75.11	75.11	84.13	56.47
10	1	0	0	0	0.00	0.00	67.17	68.04	0.00	0.00	0.00
10	2	0	0	0	0.00	0.00	68.04	69.16	0.00	0.00	0.00
10	3	0	0	0	0.00	0.00	69.16	70.13	0.00	0.00	0.00
10	4	0	0	0	0.00	0.00	70.13	71.05	0.00	0.00	0.00
10	5	0	0	0	0.00	0.00	71.05	72.04	0.00	0.00	0.00
10	6	0	0	0	0.00	0.00	72.04	73.18	0.00	0.00	0.00
10	7	1	375	1	17.12	70.38	17.12	74.04	0.00	0.00	0.00
10	8	0	0	0	0.00	0.00	74.04	75.11	0.00	0.00	0.00
11	0	1	275	1	7.85	35.91	7.85	35.91	35.91	125.20	56.47
11	1	0	0	0	0.00	0.00	26.53	27.69	0.00	0.00	0.00
11	2	1	275	1	7.85	35.91	7.85	35.91	0.00	0.00	0.00
11	3	0	0	0	0.00	0.00	28.61	29.51	0.00	0.00	0.00
11	4	0	0	0	0.00	0.00	29.51	30.35	0.00	0.00	0.00
11	5	0	0	0	0.00	0.00	30.35	31.34	0.00	0.00	0.00
11	6	0	0	0	0.00	0.00	31.34	32.21	0.00	0.00	0.00
11	7	0	0	0	0.00	0.00	32.21	33.33	0.00	0.00	0.00
11	8	0	0	0	0.00	0.00	33.33	34.44	0.00	0.00	0.00
-99999	0	0	0	0	0	0	0	0	0	0	0

Appendix A

Development of Wind-Wave Erosion Parametric Equations

Development of Wind Wave Erosion Parametric Equations

The erosion curve (time versus erosion) is specifically defined for each island sector. The erosion curves are developed for groups of island sectors that have similar levee geometry and material, fetch and exposure. The seasonal (two seasons) curves will be developed by separate analysis outside of the main risk assessment and, once developed, will be included in the ER&R module.

Episodic events do not need to be explicitly included in the ER&R module for purposes of secondary damage (erosion) computation. This removes unnecessary complexity from the model by eliminating a need for interface with the wind hazard module. Each erosion curve, or parametric equation, is developed by incorporating seasonal conditions and episodic events into the analysis.

Separate analysis that we have carried out indicates that both seasonal and episodic events contribute to levee erosion. The analysis also demonstrates that, over time, the waves generated by the seasonal winds are the more significant contributor to levee interior slope erosion. Since the episodic events are not significant contributors to levee interior slope erosion, the problem can be simplified significantly by treating these events in a separate analysis and incorporating their effect into the erosion curves rather than treating them as separate events in the ER&R model. Because of their lesser importance in the computation of ongoing damage on already flooded islands, they are not necessarily required in the ER&R module.

The development of the erosion curves, or parametric equations, was carried out outside of the ER&R module. Its main objective is to develop a set of erosion curves, or parametric equations, which will be input into the ER&R module to accumulate erosion damage over time as repairs progress.

- 1. Develop a relationship between levee erosion rate and wind-wave height, which includes uncertainty.
- 2. Analyze historical wind data and develop wind roses (for long-term erosion calculation) and extreme wind events (return period wind speed and duration, for episodic wind wave erosion calculation) for each of the eight directions (N, S, E, W, NW, NE, SW, SE). This work is to be carried out by Phillip Williams and Associates. The available wind stations include Sacramento Airport, Stockton Airport, Bethel Island (Bay Area Air Quality Management District station), Pittsburg Power Plant or Port Chicago (NOAA station). The entire Delta area can be divided into four regions, each of which will be represented by one of the wind stations.
- 3. Generate a random wind time history for a period that covers the period of repair (say 10 years), based on results from (2).
- 4. Calculate wind waves using results from (3), for a number of fetch distances.



- 5. For each fetch distance, calculate cumulative levee erosion over time based on results from (4) and (1) along each individual wind direction. For each wind direction, the entire perimeter length of the opposing island sector will be assumed to be subject to erosion.
- 6. Repeat (3), (4) and (5) multiple times (say 100), and develop averaged levee erosion over time with the 1-standard deviation upper bound and lower bound as well, for each wind direction and for each of the fetch distances specified above.

The analyses will be carried out on one or two typical levee cross sections. Levee material is assumed to be compacted silty sand. The result of the set of analyses will be a database that can be used within the ER&R module.

The underlying assumption is that wind-driven waves will be fully developed within 1 hour.

Relationship between Levee Erosion Rate and Wind-Wave Height

Estimating wind-wave induced damage to flooded Delta island levees requires a means of correlating wave heights to erosion rates. Many studies have investigated levee or shoreline erosion due to waves or other scour processes (Elci et al. 2002; Foda et al. 1999; Hanson and Cook 2006; Hanson and Hunt 1999; Seed et al. 2006). Erosion processes are complex and involve numerous dependencies; thus, many investigations utilize approaches that require calibration to site-specific hydraulic boundary stresses, soil properties and other parameters such as vegetation. Because no experimental or field erodibility data was available to this study, a range of approaches and assumptions was utilized in attempt to "book-end" or bracket the likely expected envelope of erosion.

The stress-based detachment equation (also referred to as excess stress equation) was used to calculate the time rate of erosion under wave stresses (Hanson and Cook 2006; Hanson and Hunt 1999). The equation states that the erosion rate is a function of a soil detachment coefficient, a wind/wave-induced hydraulic boundary stress, and a critical soil stress required to initiate material detachment

$$\varepsilon = k_d (\tau - \tau_c) \tag{1}$$

where:

 ε = erosion rate in volume per unit area per unit time (ft/hr)

 k_d = detachment rate coefficient, a soil material property (ft³/lb-hr)

 τ = hydraulically applied boundary stress (lb/ft²)

 τ_c = critical soil shear stress for erosion, a soil material property (lb/ft²).



Development of Wind Wave Erosion Parametric Equations

The hydraulic boundary stress, τ , in Equation (1) was calculated using a boundary shear stress formulation, whereby the boundary stress is a function of wave height under pure wave environments (Fredsoe 1981 in DHI 1996). The formulation states:

$$\tau = \frac{1}{2} \rho f_w U_b^2 \tag{2}$$

where:

 ρ = density of the fluid (lb/ft³) f_w = wave friction factor (unitless) U_b = horizontal mean orbital wave velocity at water-soil interface (ft/s)

The wave friction factor is an empirically based function of the mean orbital motion at the bed, wave properties including the wave height and period, and a roughness-friction factor. The orbital wave velocity, U_b , is dependent on the significant wave height, the wave period, and the water depth.

Because the boundary shear stress approximation is generally suitable for slower erosion of softer bottom sediments like those of a lake or river bed, it may underestimate erosion of shorelines or levee embankments that are often under-cut and incised, eroding irregularly over time. To consider the eroding forces of waves directly impacting a sloped levee surface, a wave force method was also utilized to approximate the erosive shear stress (USACE 2001). This method is a physically based approach to approximate horizontal forces of shallow water waves. This alternative procedure also relates wave height to hydraulic bed shear stress by integrating the wave force over the length of the wave to calculate an average erosive force per unit area of levee in the direction of the levee slope.

The soil dependent variables in Equation (1) are τ_c and k_d . These are used to represent the range of parameters that affect soil erodibility:

- Soil gradation
- Compaction
- Water content
- Dry density

In erosion modeling studies, the values of these soil parameters range widely. Sands and clays can show variations of several orders of magnitude. For the purposes of this investigation, levee material is assumed to be a relatively firm soil that is predominately clay with some silt. For soils of this type, the parameters k_d and τ_c can range as shown in Table A-1.

Development of Wind Wave Erosion Parametric Equations

Table A-1 Soil Erodibility Parameter Ranges

Lower Limit	Upper Limit
0.1 cm 3/N-s	0.3 cm3/N-s
(1.6E-5 ft3/lb-s)	(4.7E-5 ft3/lb-s)
5 Pa (0.11 lb/ft²)	12 Pa (0.25 lb/ft^2)
	0.1cm3/N-s (1.6E-5 ft3/lb-s) 5 Pa

Source: Hanson and Cook 1999; Hanson and Hunt 2006.

The resulting erosion calculations are plotted on Figure A-1. The discrete points, "erosion samples" (blue dots), were calculated by the two different wave stress methods and by using the upper and lower limits of the soil parameters. Based on these discrete erosion points, an upper and lower envelope was defined by calculating the plus one and minus one standard deviation about the mean erosion rate. The shaded region on Figure A-1 is the envelope of likely erosion rates under varying wave conditions.

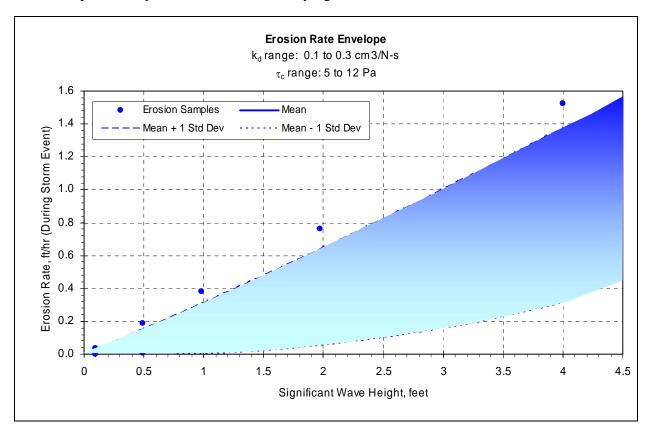


Figure A-1 Erosion Rate Envelope

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